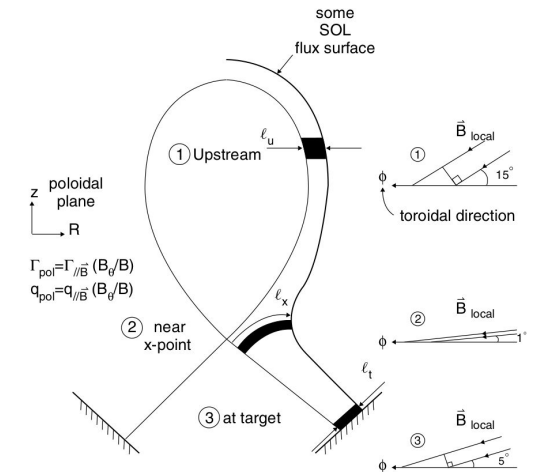


# Advanced methods for tokamak heat load studies

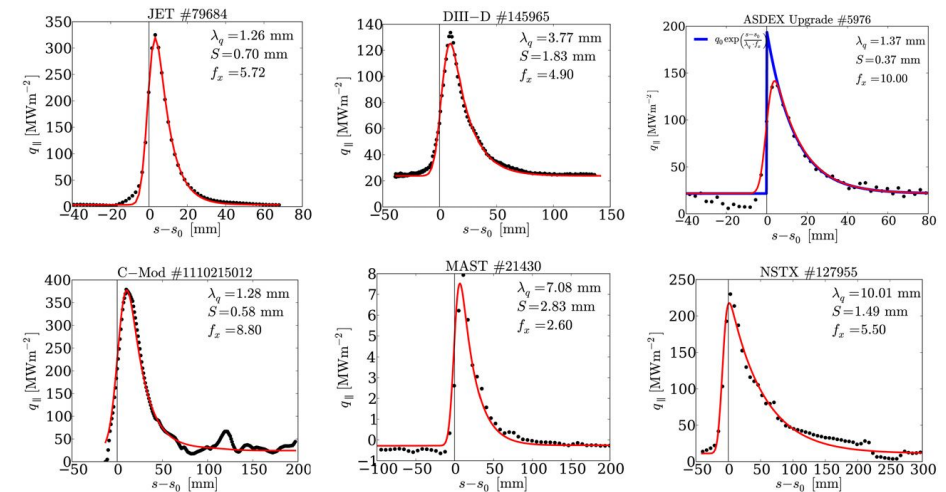
Jakub Čaloud

## Tokamak first wall heat loads

- First wall of tokamak will be exposed to extreme heat loads - one of the unsolved challenges for fusion reactors
- Stationary plasma heat loads ( $q$ ):
  - Directed at small area on the divertor
  - $q \sim 10 \text{ MW/m}^2$  in ITER - limited by material parameters
- Transient heat loads:
  - ELMs:  $q \sim 1 \text{ GW/m}^2$ ,  $t < 1 \text{ ms}$
  - Disruptions:  $q \sim 10 \text{ GW/m}^2$ ,  $t = 1 - 10 \text{ ms}$
  - Runaway electrons:  $q < 1 \text{ GW/m}^2$
- Transient thermal loads can lead to irreversible material degradation and tokamak damage
- Heat load measurements are important for safe tokamak operation and development of heat load mitigation techniques



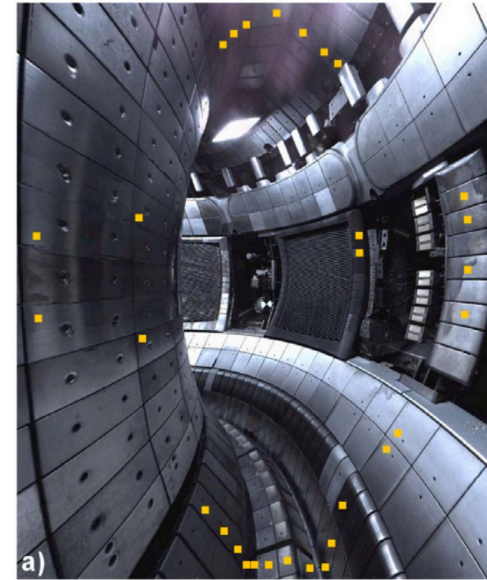
P C Stangeby et al.: The plasma boundary of magnetic fusion devices



T Eich et al.: Nucl. fus. 53(9):093031, 2013

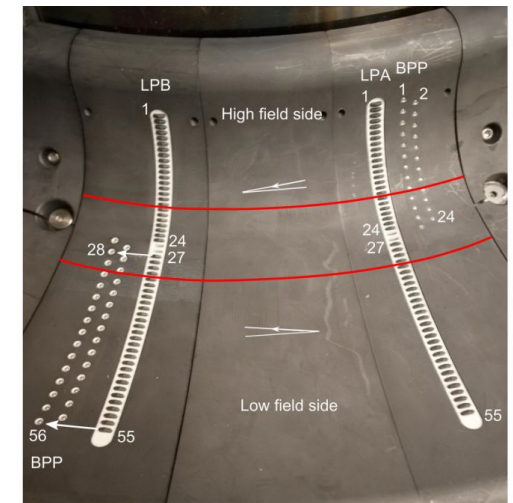
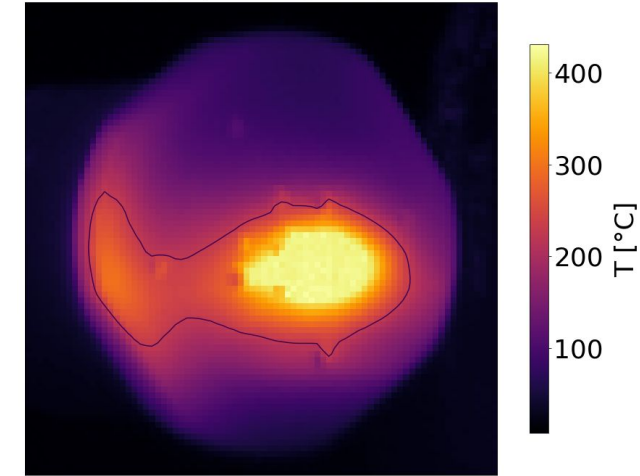
## Plasma heat flux diagnostics

- PFC calorimetry
  - Deposited energy estimated from temperature change of the PFC tiles measured by temperature sensors
  - Heat flux profile estimated from multiple sensors
- IR thermography
  - Heat flux estimated IR camera measurements of surface temperature - heat diffusion equation
- Electrostatic probes
  - Heat flux determined from edge plasma parameters  $T_e$ ,  $n_e$  measured by probes



T Hohmann et al.: Fus. Eng. Des. 187 (2023): 113365

#20054, t = 1524.8 ms



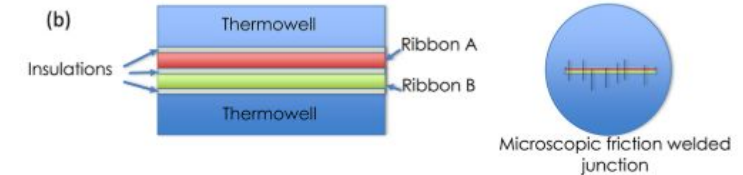
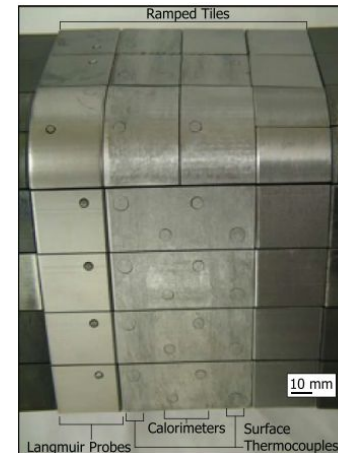
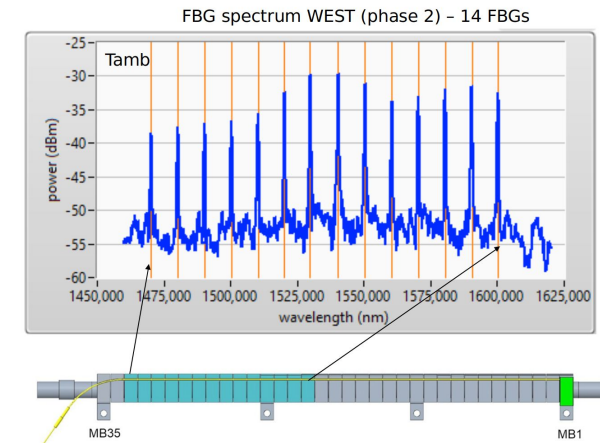
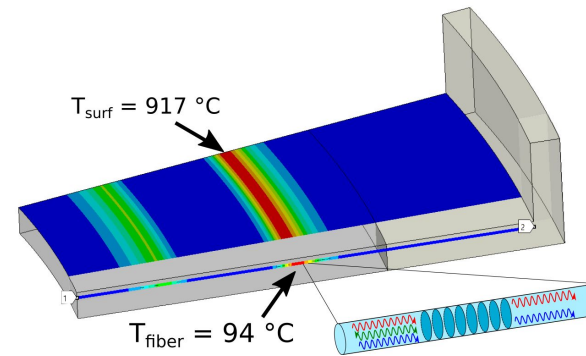
J Adamek et al.: Nucl. Fus. 57.11 (2017), p. 116017

## Calorimetry diagnostics for COMPASS-U

- FBG thermal diagnostics
  - Based on Fiber Bragg Grating temperature sensors
  - Heat load estimation and profile measurements
  - Conceptual design in progress
  - Inner limiter and initial divertor for plasma heat loads
  - Outer limiter considered for transient and RE heat load measurements
  
- Surface thermocouples proposed for later phases
  - Self-renewing thermocouple junction on the surface
  - Heat flux measurements from surface temperature changes

$$\lambda_B = 2n_{\text{eff}}\Lambda$$

$$\Delta\lambda_B = 2 \left( \Lambda \frac{\partial n}{\partial l} + n_{\text{eff}} \frac{\partial \Lambda}{\partial l} \right) \Delta l + 2 \left( \Lambda \frac{\partial n}{\partial T} + n_{\text{eff}} \frac{\partial \Lambda}{\partial T} \right) \Delta T$$



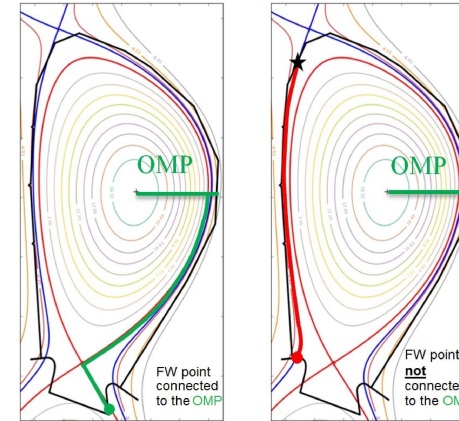
Brunner, D., and LaBombard B., Rev. Sci. Instrum. 83.3 (2012): 033501

## PFCFlux heat load simulations

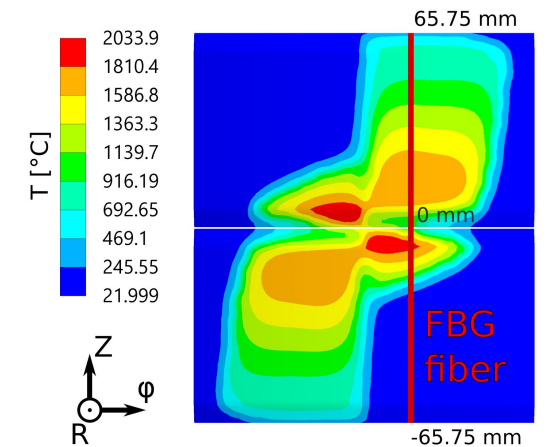
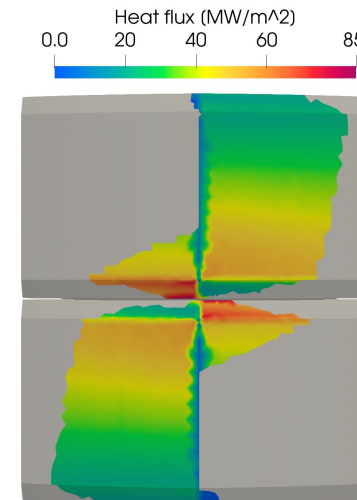
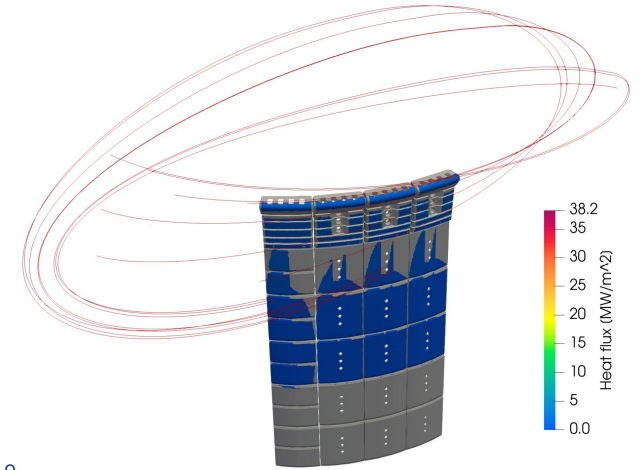
- 3D heat flux and shadowing simulations by field line tracing
- Optimization of PFC shape, scenario development and diagnostics design

## ANSYS FEA thermal analysis

- Finite element analysis (FEA) of temperature evolution
- Solving 3D transient heat conduction equation
- Inputs:
  - PFCFlux - surface heat flux from plasma
  - FLUKA - volumetric RE heat loads

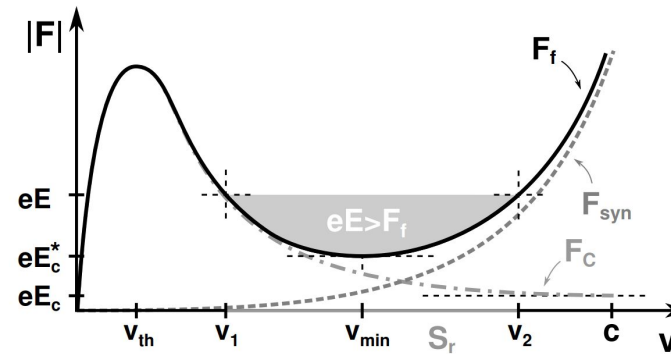


J Gerardin et al.: Nucl. Mater. Energy 20:100568, 2019

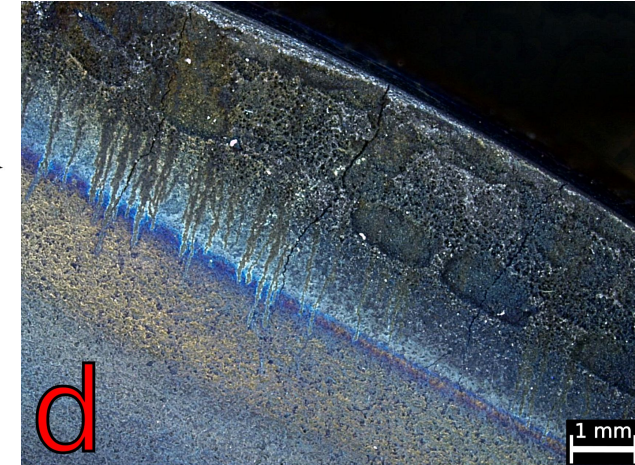
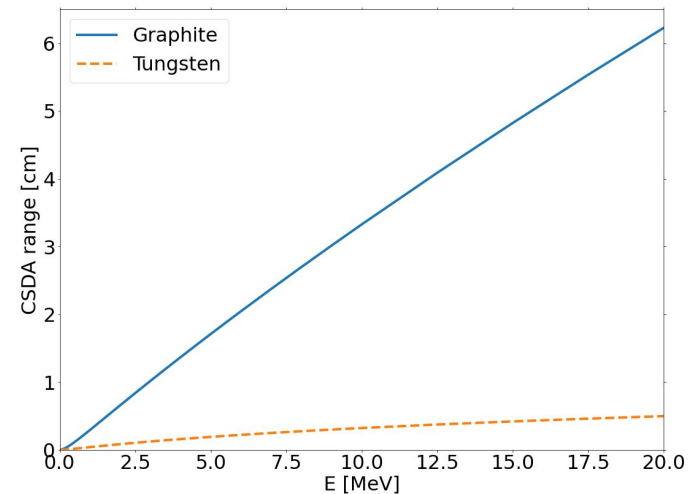


## Runaway electron heat loads

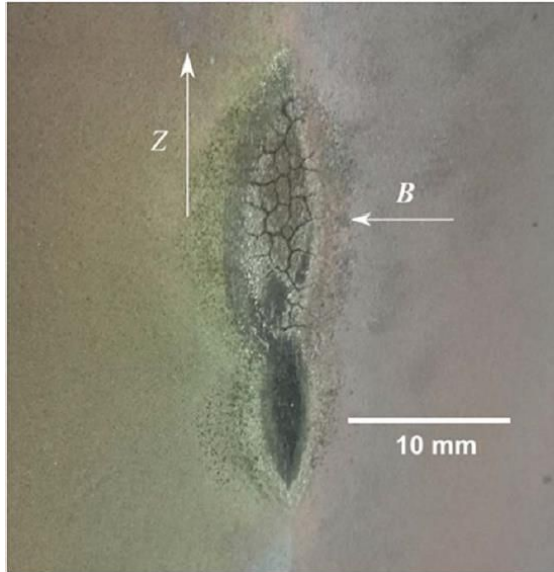
- Runaway electrons (RE) - electrons accelerated to relativistic velocities by electric field
- Kinetic energy up to tens of MeV ( $> 90\% c$ )
- Possible damage to tokamak
  - heat loads in tens of  $\text{MW}/\text{m}^2$  (at COMPASS)
- Development of mitigation techniques necessary
- RE kinetic energy lost by collisions and bremsstrahlung  
 -> energy deposition up to several cm in PFC material



A. Stahl, PhD thesis, 2017

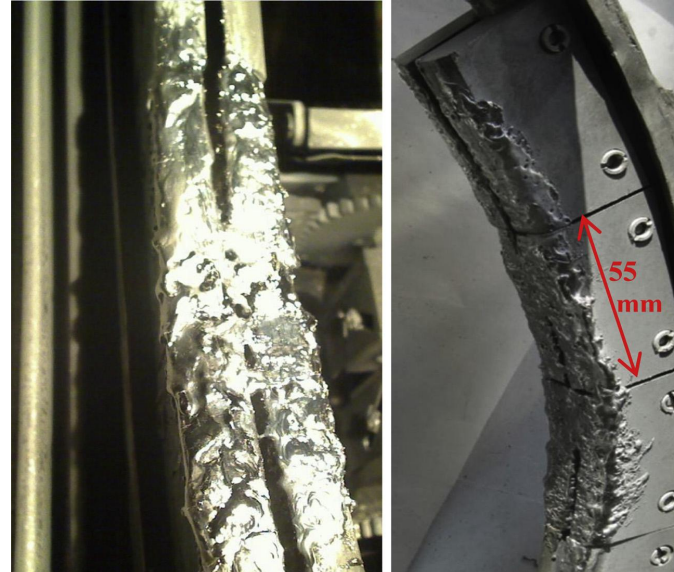


COMPASS



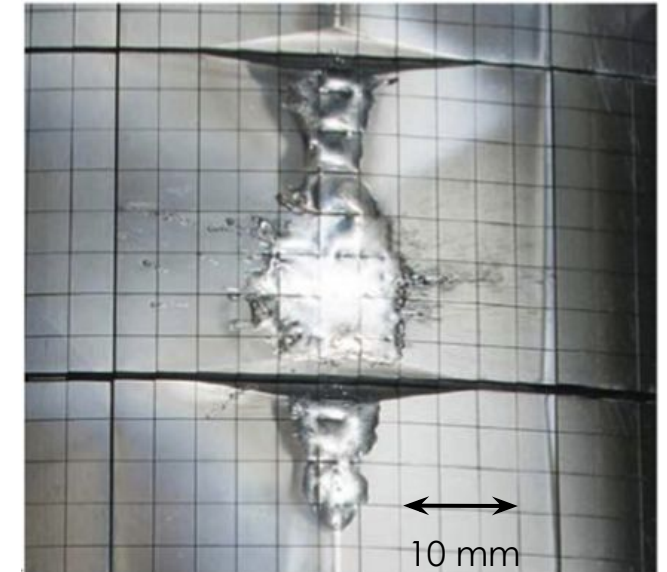
$E_{RE} < 10 \text{ MeV}$   
 $I_{RE} = 100 \text{ kA}$   
 $E_{max} = 15 \text{ kJ}$   
 $q_{max} = 30 \text{ MW/m}^2$

T-10



$E_{RE} < 2 \text{ MeV}$   
 $I_{RE} < 200 \text{ kA}$   
 $q_{max} = 1 \text{ GW/m}^2$   
 Damage after 500 disruptions

JET



$E_{RE} < 20 \text{ MeV}$   
 $I_{RE} < 2 \text{ MA}$   
 $E_{max} = 1.5 \text{ MJ}$   
 $q_{max} = 400 \text{ MW/m}^2$

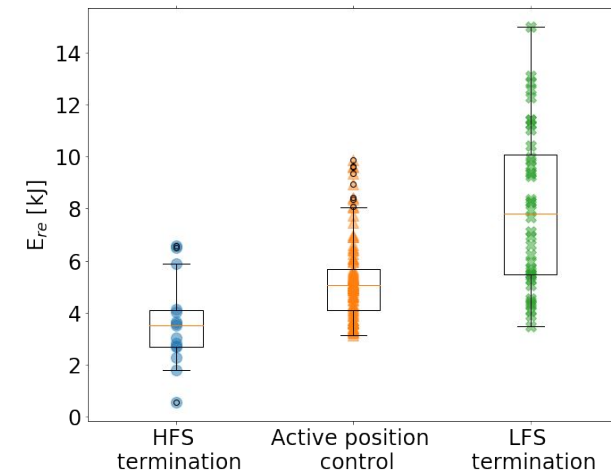
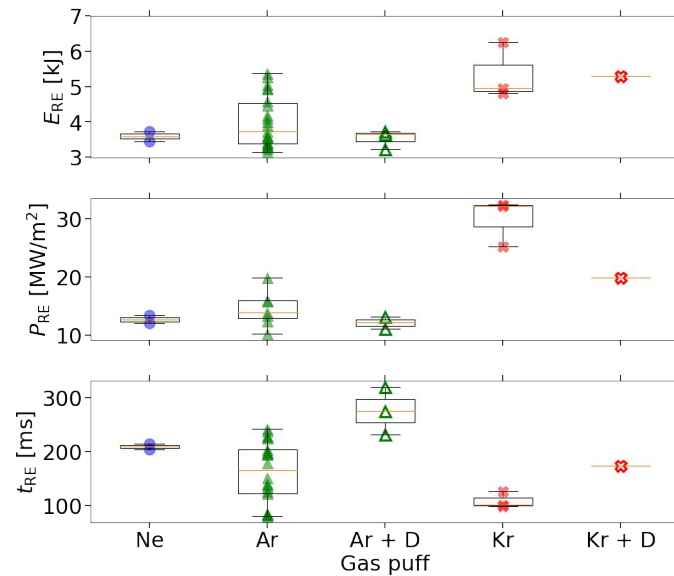
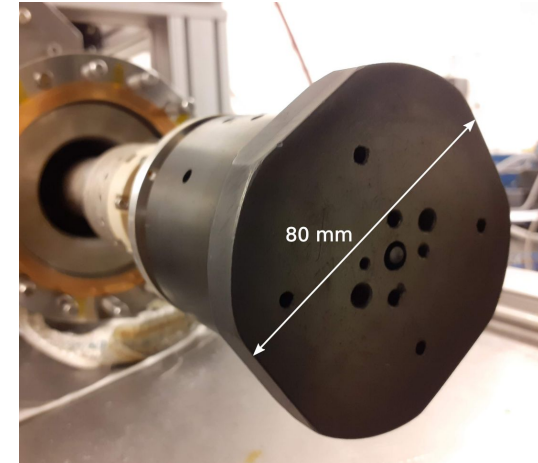
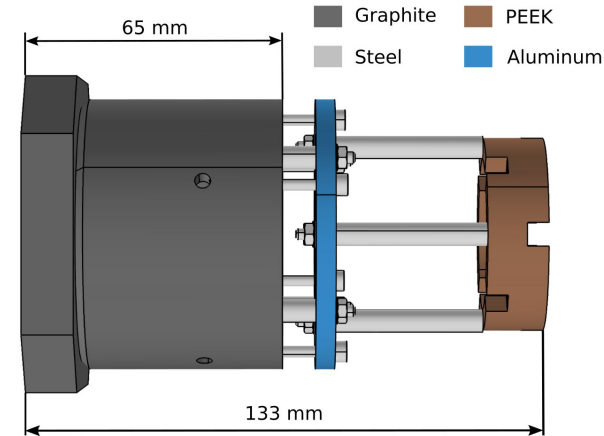
**COMPASS-U** estimated:  $I_{RE} > 100 \text{ kA}$ ,  $E_{RE} < 20 - 25 \text{ MeV}$

**ITER** estimated:  $E_{max} = 300 \text{ MJ}$ ,  $q_{max} < 1 \text{ GW/m}^2$

J Mlynar et al.: Plasma Phys. Control. Fusion 61.1 (2018): 014010  
 S Grashin et al.: Fus. Eng. Des. 146 (2019): 2100-2104  
 G Matthews et al.: Phys. Scr. 2016.T167 (2016): 014070

## Runaway electron calorimetry at COMPASS

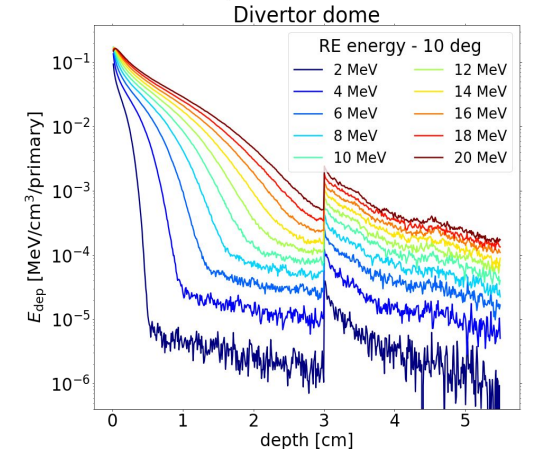
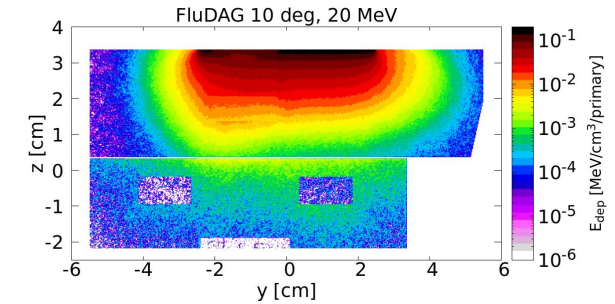
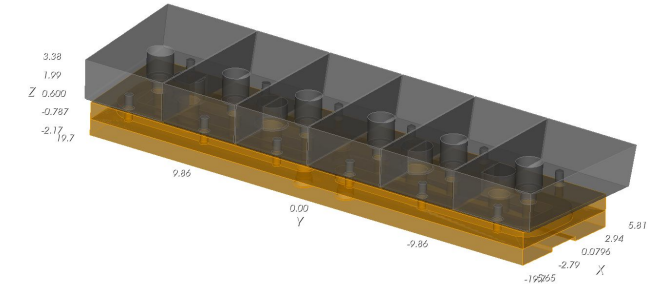
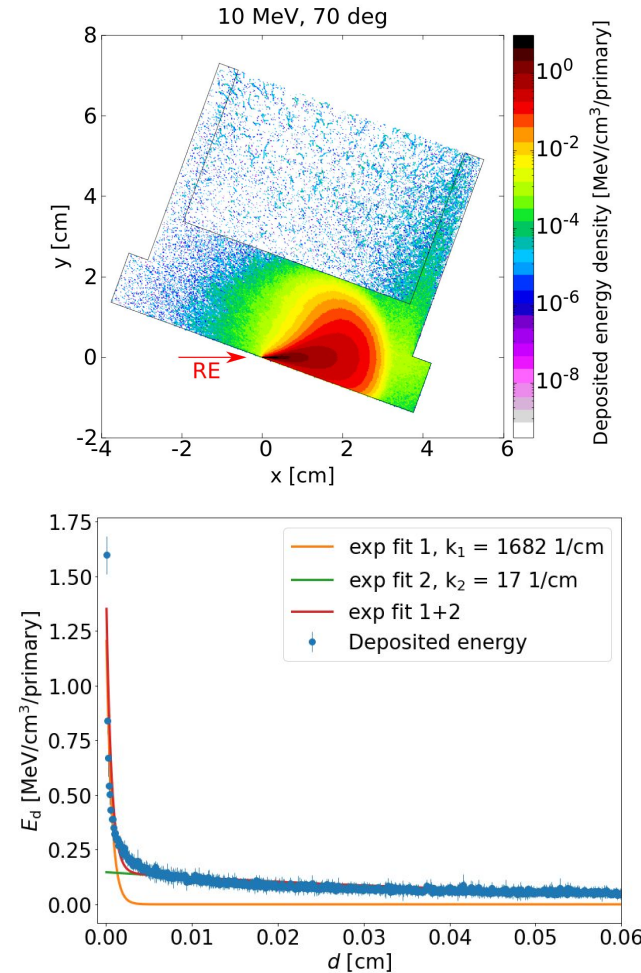
- RE calorimetry probe - master thesis project
- COMPASS LFS protection limiter equipped with temperature sensors for RE heat load measurements
- RE heat loads estimated from temperature sensors and IR measurements
- Measured effects:
  - Impurity injection (gas and pellets)
  - RE beam termination position
  - Additional RE drive





## FLUKA Monte Carlo simulations

- Monte Carlo code for interaction and transport of high energy particles
- Modelling of energy deposition by runaway electrons in the PFC material
- Results can be exported to ANSYS for thermal analysis
- RE impact simulated for:
  - COMPASS RE calorimeter
  - COMPASS-U outer limiters
  - JT-60SA limiters and divertor
  - Planned: WEST calorimetry divertor tiles damaged by RE impact



## Summary

- First wall thermal measurements important for safe tokamak operation and development of heat load mitigation techniques
- Predictive modelling needed for scenario development, optimization of plasma-facing components and diagnostics development
- Commonly used plasma heat flux diagnostics:
  - PFC calorimetry
  - IR thermography
  - Electrostatic probes
- Plasma heat flux simulations:
  - Field line tracing - heat flux distribution
  - Heat conduction - temperature change
- Runaway electron heat loads can damage plasma-facing components
- Calorimetry diagnostics and predictive modelling can be used for development of mitigation strategies